



# Investigation on inkjet printing for electromagnetic compatibility application

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## Keywords

Inkjet printing, high accuracy, electromagnetic compatibility (EMC), frequency-dependent attenuation of electromagnetic waves

## Abstract

The research focused on the development of inkjet-printed silver grids on flexible films to (I) attenuate electromagnetic waves at 2.45 GHz locally by applying them directly on Wi-Fi or Bluetooth transmitter or to (II) protect electromagnetic compatibility (EMC) sensitive devices close to electromagnetic transmitters. The inkjet printing technology leads to resource, time as well as cost efficient manufacturing and simplifies the adjustment of the pattern design regarding different applications. The research contains a fundamental analysis of the behavior of printed silver patterns on flexible polymer substrates regarding line widths, layer morphology and electrical performance. On that basis, the grid pattern for a certain frequency range is simulated. The report shows first simulation results on basis of the given material parameters. The results are the fundamentals for further research on realization of the simulated grid patterns by inkjet printing technology.

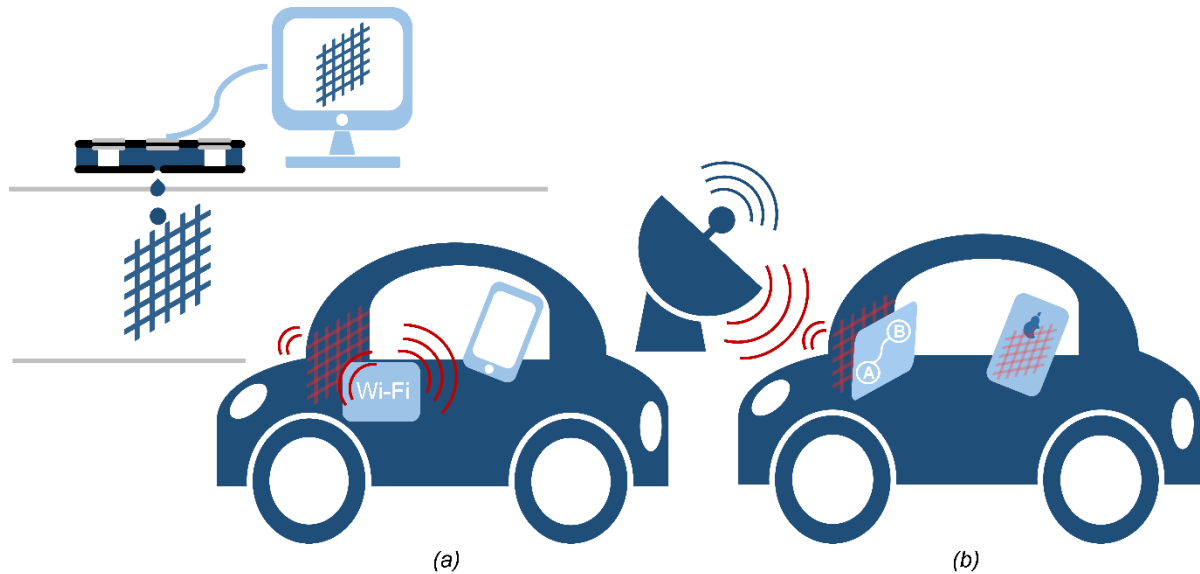
## 1 Introduction

The inkjet printing technology is an additive and therefore economic manufacturing process, since the material is applied only on areas where it is needed. Electronic devices like resistors, capacitors [1], antennas [2] and further functional thin film patterns can be realized with small amounts of material. Due to the fact that it is a digital and contactless printing technology the layout can easily be adjusted for different purposes on the one hand and on the other hand various substrates especially flexible ones can be used and roll-to-roll processed. This circumstances lead to the possibility to combine the printing process with various manufacturing methods e.g. to produce smart lightweight composites [3].

In this research inkjet-printed silver grids are investigated with regard to accurate line geometries which are given by simulations. The challenge is to realize printed patterns which deviate from the simulated ones as less as possible to realize a defined and reproducible attenuation or shielding especially at high frequency ranges [4]. Two possible applications are considered. On the one hand the attenuation of electromagnetic radiation of commercial devices like Wi-Fi and Bluetooth applications (e.g. in automobiles) in a specified frequency range to protect these wireless networks from unwanted external access as well as disturbances. On the other hand to ensure a protection of EMC sensitive devices close to electromagnetic transmitters with high output power (e.g. radar, magnetic resonance tomography). Figure 1 demonstrates schematically the manufacturing process and the two potential applications of the printed silver grids.

State of the art demonstrates that there is a need of electromagnetic shielding especially from healthcare and data security point of view [5, 6]. To replace currently used complex manufacturing processes e.g. conventional printed circuit board technologies like chemical etching [7, 8] and spray coating [9] or thick

screen printed layers [10], the inkjet printing technology has great potential to fulfill the requirements of minimal material input by narrow patterns and small layer thickness with simultaneous performance accuracy.



*Figure 1: Manufacturing process of inkjet-printed grid and the potential application as (a) electromagnetic wave attenuator or (b) protector of EMC sensitive devices*

## 2 Experimental

### 2.1 Printing Process and Materials

The inkjet-printing process was performed with a Dimatix Materials Printer (DMP) 2831 and an installed piezoelectric printhead with 16 nozzles, which have a distance of 254  $\mu\text{m}$  (Figure 2). The piezoelectric elements are driven by a voltage waveform. A silver nano-particle ink PE410 (DuPont) was used and printed on a PET substrate Melinex 506 (DuPont Teijin Films) which has a thickness of 100  $\mu\text{m}$ . The solid content of the ink is 45.2 wt% dissolved in Butyldiglycol and octylamine [11]. The PET substrate consists of an adhesion promoting pre-treatment [12].



*Figure 2: Dimatix Inkjet Printing System DMP 2831 and Cartridge with Printhead [13]*

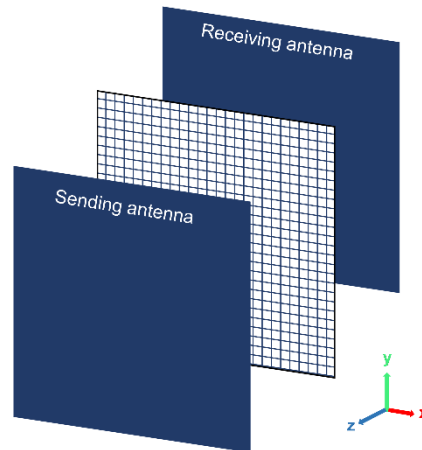
Preliminary experiments were implemented to evaluate the performance of the ink at different resolutions, which are defined by the drop space (DS) (distance of the deposited droplets). One pixel (px) lines with DS 15 to 45  $\mu\text{m}$  were printed as well as 300  $\mu\text{m}$  wide lines and 5 x 5 mm<sup>2</sup> squares with ideal DS for electrical characterization.

The printed layers have to be sintered to evaporate the solvent, to cast out the organic non-conductive components and to encourage a grain growth. To form dense and conductive layers the samples were sintered in a convection oven for 60 min at 100 °C.

On the basis of the morphological and electrical evaluation of the preliminary experiments the grid pattern was simulated.

## 2.2 Simulation of Pattern Design

The grid pattern for the frequency-dependent attenuation of electromagnetic waves was simulated by the software CST Microwave Studio Suite [14]. The built up simulation design can be seen in Figure 3.



*Figure 3: Simulation design - simulated grid between sending and receiving antenna*

A grid pattern was chosen intentionally because of less material consumption compared to conventional full-surface coating and the aim to customize the layout design to different frequency ranges.

## 2.3 Characterization

The printed lines as well as squares were analyzed optically by microscopic images (Leica DM 4000 M), morphologically by surface profile measurement (Veeco Dektak 150) and electrically by sheet resistance measurements (5 x 5 mm<sup>2</sup> squares) by the four point Van-der-Pauw method. These measurements reveal the optimal DS to be used to reproduce the simulated pattern precisely and reliably. Open layers, blurred edges and inaccurate dimensions could affect the target design of the grid. Therefore, accurate dimensions and sharp edges are crucial.

# 3 Results and Discussion

## 3.1 Preliminary Experiments

First of all, an optical analysis of patterns printed with different DSs was implemented. As the microscopic images (Figure 4 (a)) show, the width of the lines seems to decrease by larger DSs. Since fewer droplets are deposited if a higher DS is used less material is applied onto the substrate. Due to the fact that closed, sharp and fine patterns with DS 30 to 40 µm could be realized 300 µm wide lines and 5 x 5 mm<sup>2</sup> square patterns are printed with DS 30 and 40 µm. These DSs seem to form close and dense layers (Figure 4 (b) and (c)).

To confirm the optical impression the line width and layer profile measurements are performed subsequently.

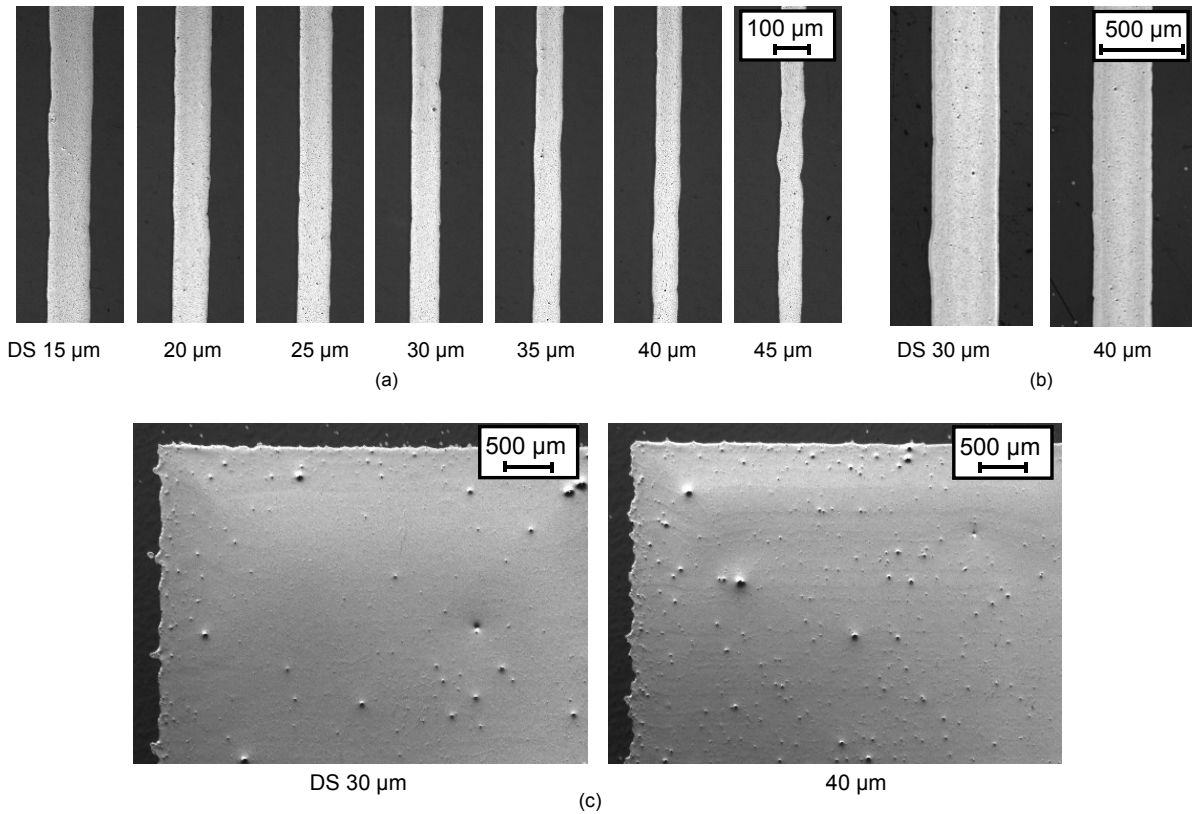


Figure 4: Microscopic images of (a) 1 px lines, (b) lines of 300  $\mu\text{m}$  width and (c) 5 x 5 mm<sup>2</sup> squares printed with different DS

The line width measurements (Figure 5 (a)) confirm that increasing DSs lead to reduced line widths.

For printing the 300  $\mu\text{m}$  wide lines DSs of 30 and 40  $\mu\text{m}$  were used (Figure 5 (b)). It can be noticed that the printed line widths differ from the nominal line width (300  $\mu\text{m}$ ). This fact has to be considered in the subsequent simulation of the grid pattern.

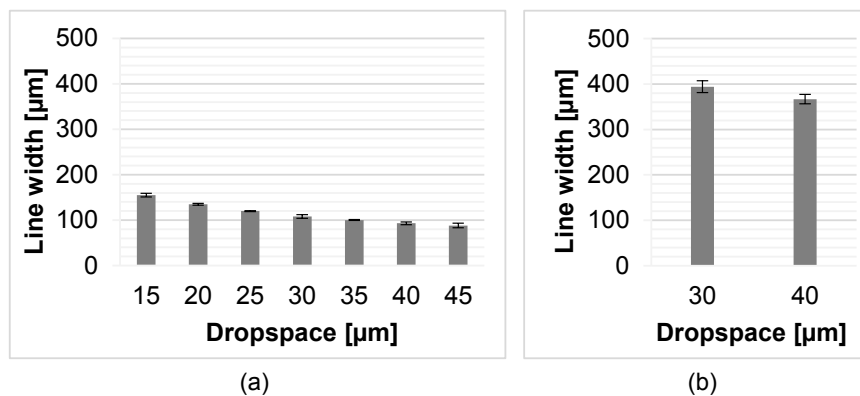


Figure 5: Average line width of (a) 1 px lines and (b) 300  $\mu\text{m}$  wide lines printed with different DS

Figure 6 demonstrates the layer morphology (a) and average layer height (b) of the printed 1 px and 300  $\mu\text{m}$  wide lines. Higher DSs obviously lead to a decreased layer thickness since less material is applied onto the substrate. If 1 px lines and 300  $\mu\text{m}$  wide lines are compared it can be seen that the layer height increases with broader patterns. The 1 px lines also show a so called coffee-ring effect, this means more material is located at the edges of the lines. This effect is reduced in case of wider lines.

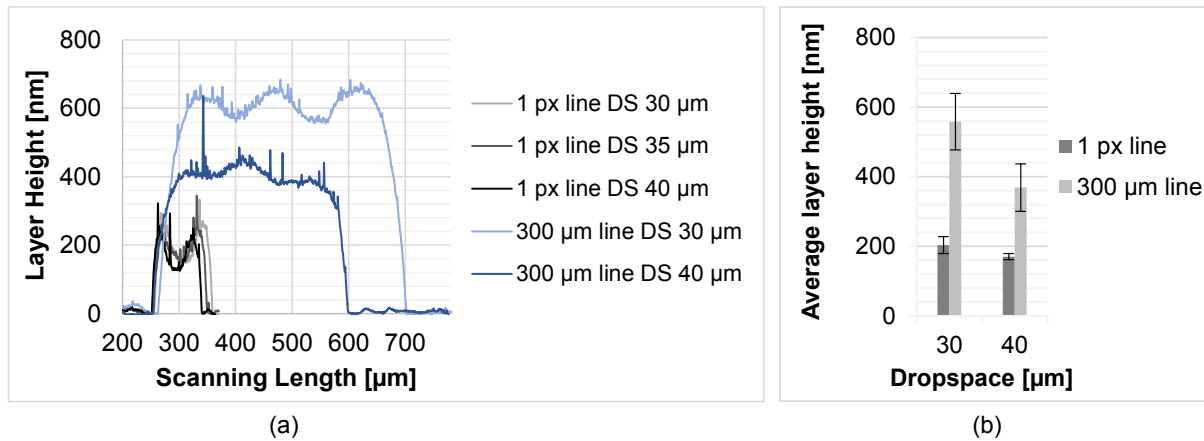


Figure 6 : (a) Surface profile and (b) Average layer height of 1 px lines and 300  $\mu\text{m}$  wide lines printed with different DS

The electrical evaluation of the preliminary printed patterns confirm the previous optical and morphological measurement results. The resistance increases by increasing DS (Figure 7) due to a smaller amount of deposited material. Nevertheless, the sheet resistance values of DS 30 and 40  $\mu\text{m}$  differ only slightly from each other. The electrical properties of the patterns seem sufficient for the intended simulated pattern design and the application later on.

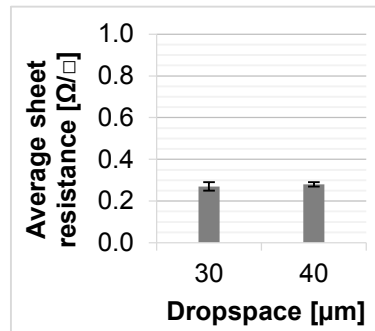


Figure 7: Average sheet resistance of patterns printed with different DS

### 3.2 Simulation results

Lines with a nominal width of 300  $\mu\text{m}$  and an average printed width of 367  $\mu\text{m}$  (DS 40  $\mu\text{m}$ ) respectively are considered for the simulation. The specific electrical conductivity of  $9.68\text{E}+06$  S/m used for the simulation was calculated with the help of the average line thickness (369 nm) and the average sheet resistance ( $0.28 \Omega/\square$ ) of the printed layers. These values were the basis for the simulation of a grid pattern with different mesh widths at a resonance frequency between 1 and 10 GHz (Figure 8).

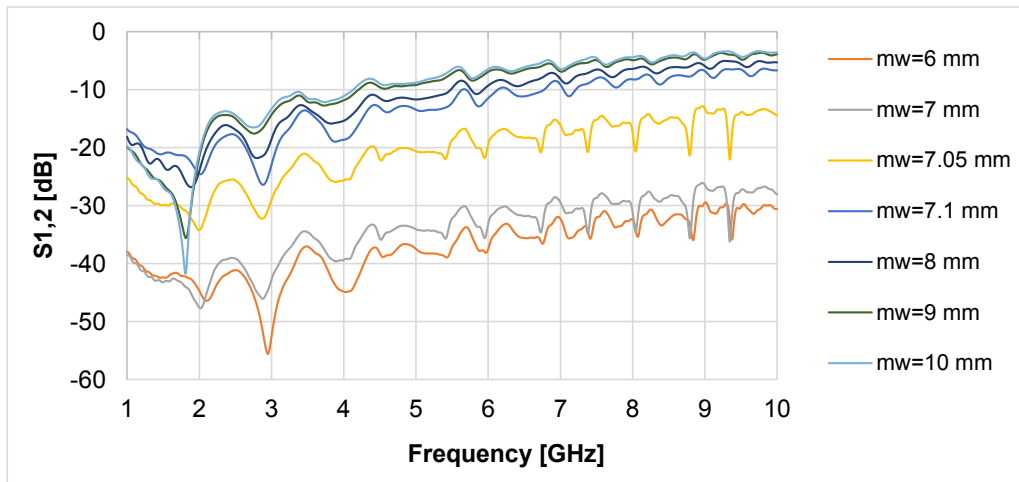


Figure 8: Frequency-dependent attenuation at different mesh widths (mw)

The simulation shown in Figure 8 demonstrates that with decreasing mesh width (mw) the attenuation effect of the resonance signal increases. There is a noticeable jump in the attenuation between mesh width 7.1 mm and 7.05 mm as well as from 7.05 mm to 7. While the attenuation effects of grids with mesh widths in the range of 7.1 to 10 mm are only slightly different. All in all, it is demonstrated that a frequency dependent attenuation between -10 and -50 dB is achievable with the given material parameters.

Additionally, the attenuation dependency on the width of the grid lines was simulated (Figure 9).

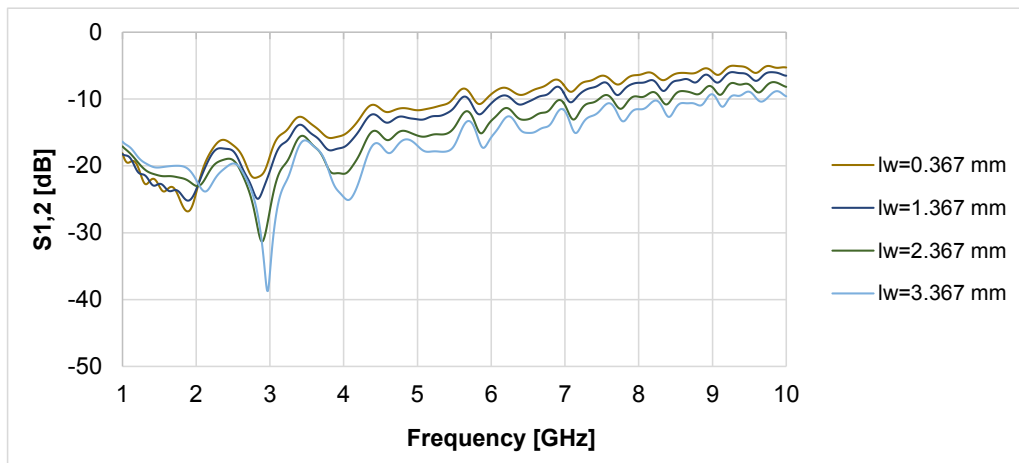


Figure 9: Frequency-dependent attenuation at different line widths (lw), constant mesh width of 10 mm

The simulation shown in Figure 9 demonstrates that the line width (lw) of the grid lines has no relevant influence on the attenuation of the resonance signal. Which will be considered in further research.

All in all the simulations show that with changing of either line or mesh width of the grids an intended attenuation can be realised at various frequencies leading to various application possibilities.

## 4 Conclusion

In this research a brief characterization of a silver inkjet ink regarding line width, layer thickness and electrical performance was performed. On the basis of these fundamental experiments simulations of grid designs for the specific attenuation of electromagnetic signals were implemented. The simulation results demonstrate that the utilized silver ink has great potential to be used for grid patterns attenuating

electromagnetic waves. The mesh design with narrow line widths as well as thin layers which can be realized especially by the inkjet printing technology lead to minimal and selective material input and therefore a resource efficient manufacturing. Simulations demonstrate that the width of the printed silver lines has less influence than the mesh width of the grid. The planned printed meshes will operate at the intended frequency of 2.45 GHz and moreover at further frequencies. The results are the fundament for future researches where the simulated grids will be realized by the inkjet printing technology and applied for the proposed applications like local electromagnetic wave attenuation on Wi-Fi or Bluetooth transmitters and in future also for protection of electromagnetic compatibility (EMC) sensitive devices close to electromagnetic transmitters.

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